

105-33  
46450  
P-9

# Comparison of High Temperature, High Frequency Core Loss and Dynamic B-H Loops of Two 50 Ni-Fe Crystalline Alloys and an Iron-Based Amorphous Alloy

W.R. Wieserman  
*University of Pittsburgh at Johnstown*  
*Johnstown, Pennsylvania*

G.E. Schwarze  
*National Aeronautics and Space Administration*  
*Lewis Research Center*  
*Cleveland, Ohio*

and

J.M. Niedra  
*Sverdrup Technology, Inc.*  
*Lewis Research Center Group*  
*Brook Park, Ohio*

Prepared for the  
26th Intersociety Energy Conversion Engineering Conference  
cosponsored by ANS, SAE, ACS, AIAA, ASME, IEEE, and AIChE  
Boston, Massachusetts, August 4-9, 1991



(NASA-TM-105205) COMPARISON OF HIGH  
TEMPERATURE, HIGH FREQUENCY CORE LOSS AND  
DYNAMIC B-H LOOPS OF TWO 50 NI-FE  
CRYSTALLINE ALLOYS AND AN IRON-BASED  
AMORPHOUS ALLOY (NASA) 9 p

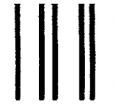
N91-32412

Unclass  
0046450

CSCL 09A 63/33

National Aeronautics and  
Space Administration

FOURTH CLASS MAIL



Lewis Research Center  
Cleveland, Ohio 44135

ADDRESS CORRECTION REQUESTED



Official Business  
Penalty for Private Use \$300

Postage and Fees Paid  
National Aeronautics and  
Space Administration  
NASA 451

**NASA**

---

# COMPARISON OF HIGH TEMPERATURE, HIGH FREQUENCY CORE LOSS AND DYNAMIC B-H LOOPS OF TWO 50 Ni-Fe CRYSTALLINE ALLOYS AND AN IRON-BASED AMORPHOUS ALLOY

W.R. Wieserman  
University of Pittsburgh  
at Johnstown  
Johnstown, PA 15902

G.E. Schwarze  
National Aeronautics and Space Administration  
Lewis Research Center  
Cleveland, Ohio 44135

J.M. Niedra  
Sverdrup Technology, Inc.  
Lewis Research Center Group  
Brook Park, Ohio 44142

## ABSTRACT

The availability of experimental data that characterizes the performance of soft magnetic materials for the combined conditions of high temperature and high frequency is almost non-existent. An experimental investigation was conducted over the temperature range of 23 to 300 C and frequency range of 1 to 50 kHz to determine the effects of temperature and frequency on the core loss and dynamic B-H loops of three different soft magnetic materials; an oriented-grain 50Ni-50Fe alloy, a nonoriented-grain 50Ni-50Fe alloy, and an iron-based amorphous material (Metglas 2605SC). A comparison of these materials shows that the nonoriented-grain 50Ni-50Fe alloy tends to have either the lowest or next lowest core loss for all temperatures and frequencies investigated.

## INTRODUCTION

Power electronic components for future high power space systems will most likely be exposed to harsh environments and will need to meet the requirements of high efficiency, low specific mass, high reliability and long life. Low system mass can be achieved by operating the power electronics at high temperature to reduce its cooling radiator mass and, also, by operating the power magnetics and capacitors at high frequency to reduce their mass.

Presently, the experimental data available to the designer on the electrical and magnetic characteristics of soft magnetic materials is almost limited to room temperature data taken under DC or 60 Hz conditions. The NASA-Lewis Research Center has

initiated an experimental program to characterize soft magnetic materials over the temperature (T) range of 23 to 300 C and frequency (f) range of 0.1 to 50 kHz for both sinusoidal and non-sinusoidal voltage excitation [1]. Previous papers have given and compared the experimental results obtained for an 80Ni-Fe crystalline alloy and two iron-based amorphous materials for T of 23 to 300 C and f of 1 to 50 kHz [2,3].

The experimental results presented in this paper are for the oriented-grain (OG) and nonoriented-grain (NOG) 50Ni-50Fe crystalline alloys. One of the amorphous materials previously reported, Metglas 2605SC, is included for comparison because it has a saturation flux density similar to the 50Ni-50Fe alloys. The experimental results reported here greatly extend the core loss and dynamic B-H loop data base for these materials. Experimental investigations of the two 50Ni-50Fe alloys reported here were also made during the late fifties [4,5,6] and late sixties [7,8]. Although those investigations included tests up to 500 C, they were done primarily under DC conditions with 3.2 kHz being the highest f reported at 250 C.

## MATERIALS AND EXPERIMENT DESCRIPTION

Table 1 gives a comparison of some of the pertinent magnetic, electrical, thermal and physical properties of the two 50Ni-50Fe alloys and the Metglas 2605SC amorphous material.

Each material was tested separately using three cores for each test. The test cores were toroids

wound from 0.001 inch thick by 0.25 inch wide tape with OD = 1.25 inches and ID = 1.0 inches. By Faraday's Law, the maximum flux density ( $B_m$ ) was calculated as the ratio of flux to core magnetic cross-sectional area ( $A_c$ ).  $A_c$  is calculated from  $A_c = (M/D\bar{l}_m)$ , where M, the mass of the core, is measured with an analytical balance, D is the magnetic material's physical density, and  $\bar{l}_m$  is the mean path length of the core determined from OD and ID. A description of the makeup of the test cores is given in Reference 2 along with a description of the instrumentation, and the equations and procedures used to obtain the test results. Every effort was made to prevent local heating of the test core by capturing the required induced voltage and exciting current waveforms in the minimum length of time. From these waveforms, the specific core loss (SCL), which is the core loss normalized to the core mass, and the B-H loop data were obtained at 1, 5, 10, 20, and 50 kHz. For each frequency, the data was taken at 23 C and then in increments of 50 C to 300 C. The data was again taken at 23 C after the material's exposure to 300 C.

## EXPERIMENTAL RESULTS

The experimental results for the OG and NOG 50Ni-50Fe and Metglas 2605SC materials are given in Figures 1 through 10. The data are for a single core and are representative of the results obtained for the three test cores of each material.

The decrease in saturation flux density ( $B_{Sat}$ ) with temperature for each material is shown in Figure 1. At 23 C the OG 50Ni-50Fe has the highest  $B_{Sat}$  of about 1.6 T, the Metglas 2605SC has slightly lower  $B_{Sat}$ , and the NOG 50Ni-50Fe has the lowest  $B_{Sat}$  of about 1.4 T. The materials retain this order from 23 to 300 C. At 300 C the  $B_{Sat}$  of the OG 50Ni-50Fe has decreased to about 1.1 T, but now both the Metglas 2605SC and NOG 50Ni-50Fe have decreased to about the same  $B_{Sat}$  value of 0.96 T.

The SCL as a function of  $B_m$  with f as the parameter is given for the OG and NOG 50Ni-50Fe and Metglas 2605SC materials in Figures 2, 5, and 8 respectively. The (a)-figures are for 23 C and the (b)-figures are for 300 C. These plots show that each material exhibits the following characteristics: For a given f, log-log plots of the SCL increase nearly linearly with  $B_m$ ; for a given  $B_m$ , the SCL increases as f increases; and for a given  $B_m$  and f, the SCL at 300 C is considerably lower than at 23 C.

Figures 3, 6, and 9 give more detail on how the SCL for these materials changes between 23 and 300 C. Here the (a)-set of figures is for  $B_m = 1.0$  T and the (b)-set is for  $B_m = 0.3$  T. These figures show that for a given f, all the materials have decreasing SCL over the entire temperature range, except that the Metglas 2605SC curves for 5, 10, and 20 kHz have a small increase in SCL between 23 and 50 C.

A representation of the dynamic B-H loops at selected frequencies for each of the three materials is shown in Figures 4, 7, and 10. The (a)-figures are for 23 C and the (b)-figures are for 300 C. To enable valid comparisons, each of the B-H loops is drawn for the same  $B_m$  of 0.9 T. Comparison of the 23 C with the 300 C loops for the same frequency, clearly shows the decrease in loop area at 300 C; this area represents the core loss per unit volume.

## MATERIALS COMPARISON

A comparison of different soft magnetic materials in terms of SCL is valid only if each material has the same physical density; otherwise, the core loss must be the basis for comparison. The 50Ni-50Fe alloys have the same density and so their SCLs can be compared. A comparison of Metglas 2605SC with the two 50Ni-50Fe alloys must be done on a core loss basis because Metglas 2605SC has a considerably lower density.

Table 2 compares the core loss of the three materials, assuming that each core has the same  $A_c$  and  $\bar{l}_m$ , and hence also the same volume. This implies that the ratio of the core masses equals the ratio of the material's densities. If the OG and NOG 50Ni-50Fe cores each weigh 1 lb., then the Metglas 2605SC core weighs 0.887 lbs. A comparison of the core losses for a given T, f, and  $B_m$  in Table 2 shows that the NOG 50Ni-50Fe alloy has the lowest losses in the majority of the cases. In the other cases, it has the second lowest loss. Thus, in most instances, the NOG 50Ni-50Fe would tend to be the material selected from core loss considerations. At 23 C and all frequencies listed, the Metglas 2605SC material needs to be considered because it has a core loss very comparable to that for the NOG 50Ni-50Fe alloy. At 150 and 300 C and for the frequencies of 20 and 50 kHz, the OG 50Ni-50Fe alloy should be considered because it has a core loss comparable to that of the NOG 50Ni-50Fe alloy.

## CONCLUSION

The experimental results for the soft magnetic materials given in this paper should enable the magnetics designer to make better decisions in the application of these materials in the temperature range of 23 to 300 C and frequency range of 1 to 50 kHz. The results in Table 2 show that the NOG 50Ni-50Fe alloy has either the lowest or next lowest core loss, so that the tendency would be to select this material. Finally, it should be noted that the experimental data presented here was obtained under very short-term temperature exposure and thus, long-term temperature exposure must be investigated to determine if ageing affects the results.

## ACKNOWLEDGMENT

This research was sponsored by the NASA Lewis Research Center under the High Capacity Power element of the Civilian Space Technology Initiative.

## REFERENCES

- [1] Schwarze, G.E., "Overview of Space Power Electronics Technology Under CSTI High Capacity Power Program," Proc. Seventh Symposium on Space Nuclear Power Systems, Conf-900109, Albuquerque, NM, January 7-10, 1990.
- [2] Wieserman, W.R., Schwarze, G.E. and Niedra, J.M., "High Frequency, High Temperature Specific Core Loss and Dynamic B-H Hysteresis Loop Characteristics of Soft Magnetic Alloys," Proc. of the 25th Intersociety Energy Conversion Engineering Conference, Reno, NV, August 12-17, 1990.
- [3] Wieserman, W.R., Schwarze, G.E. and Niedra, J.M., "Comparison of High Frequency, High Temperature Core Loss and B-H Loop Characteristics of an 80Ni-Fe Crystalline Alloy and Two Iron-Based Amorphous Alloys," Proc. Eighth Symposium on Space Nuclear Power Systems, Conf-910116, Albuquerque, NM, January 6-10, 1991.
- [4] Pasnak, M. and Lundsten, R.H., "Effects of Extremely High Temperatures on Magnetic Properties of Core Materials," U.S. Naval Ordnance Laboratory Report 6132, Silver Spring, MD, July 1958.
- [6] Fritz, J.F. and Clark, J.J., "Effects of Temperature on Magnetic Properties of Nickel-Iron Alloys Over Temperature Range -60 to 250 C," Electrical Manufacturing, November 1958.
- [7] Frost, R.M., McVay, R.E. and Pavlovic, D.M., "Evaluation of Magnetic Materials for Static Inverters and Converters," NASA Contractor Report 1226, February 1969.
- [8] Brown, A.A., Craig, H.R. and Brink, W.S., "Cyclic and Constant Temperature Ageing Effects on Magnetic Materials for Inverters and Converters," NASA Contractor Report 1468, June 1969.

Table 1. Comparison of oriented and nonoriented - grain, 50 Ni-50 Fe and Metglas 2605SC properties.			
Property	50 Ni - 50 Fe Oriented - Grain	50 Ni - 50 Fe Nonoriented - Grain	Metglas 2605 SC
Composition	50% Ni, 50% Fe <sup>(1)</sup>	50% Ni, 50% Fe <sup>(1)</sup>	Fe <sub>81</sub> B <sub>13.5</sub> Si <sub>3.5</sub> C <sub>2</sub> <sup>(1)</sup>
Structure	Crystalline	Crystalline	Amorphous
Saturation Induction	1.42 - 1.58 T <sup>(1)</sup>	1.15 - 1.40 T <sup>(1)</sup>	1.61 T <sup>(2)</sup>
Resistivity	45 x 10 <sup>-6</sup> ohm -cm <sup>(1)</sup>	45 x 10 <sup>-6</sup> ohm -cm <sup>(1)</sup>	135 x 10 <sup>-6</sup> ohm -cm <sup>(2)</sup>
Curie Temperature	500 C <sup>(1)</sup>	500 C <sup>(1)</sup>	370 C <sup>(2)</sup>
Crystallization Temp.	—	—	480 C <sup>(2)</sup>
Melting Point	1425 C <sup>(1)</sup>	1425 C <sup>(1)</sup>	1100 C <sup>(2)</sup>
Thermal Conductivity	13 w/m C <sup>(4)</sup>	13 w/m C <sup>(4)</sup>	9 w/m C <sup>(2)</sup>
Density	8.25 g/cm <sup>3</sup> <sup>(3)</sup>	8.25 g/cm <sup>3</sup> <sup>(3)</sup>	7.32 g/cm <sup>3</sup> <sup>(2)</sup>

(1) Magnetics TWC - 300 T, Design Manual Featuring Tape Wound Cores.  
(2) Allied Metglas Products, Metglas Magnetic Alloys.  
(3) The Arnold Engineering Company, TC - 101 E, Tape Wound Cores.  
(4) Carpenter, Soft Magnetic Alloys, Electronic Alloys, 11 - 88.

Table 2. Comparison of core loss of nonoriented and oriented - grain 50 Ni - 50 Fe and Metglas 2605 SC for cores having the same Ac and $\mu_m$ with the nonoriented - grain 50 Ni - 50 Fe core weight set equal to 1 lb.										
		Core Loss (w)								
f (kHz)	B <sub>m</sub> (T)	50 Ni - 50 Fe Nonoriented - Grain			50 Ni - 50 Fe Oriented - Grain			Metglas 2605 SC		
		23 C	150 C	300 C	23 C	150 C	300 C	23 C	150 C	300 C
1	.6	1.2	.80	.43	2.5	1.5	1.0	1.2	1.0	.60
1	.9	2.3	1.5	.86	4.1	2.6	2.0	2.4	1.8	1.2
1	1.2	3.6	2.4	-	5.9	3.9	-	3.9	2.8	-
5	.6	13	8.6	4.4	18	11	6.6	13	11	6.2
5	.9	24	15	8.7	30	19	13	25	19	12
5	1.2	36	24	-	42	28	-	38	28	-
10	.6	37	24	12	44	26	16	37	32	17
10	.9	64	43	25	73	47	32	66	53	32
10	1.2	96	68	-	103	70	-	99	79	-
20	.3	39	26	11	46	25	11	36	33	16
20	.6	101	69	37	108	66	41	94	80	42
50	.1	29	19	6.0	38	16	4.3	29	25	11
50	.3	151	106	48	147	88	42	151	122	63

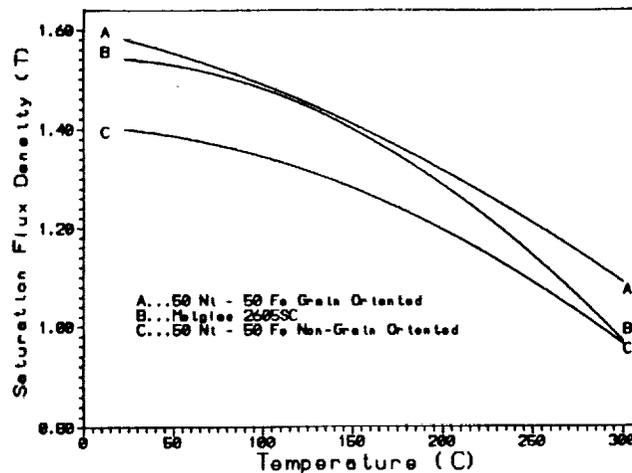
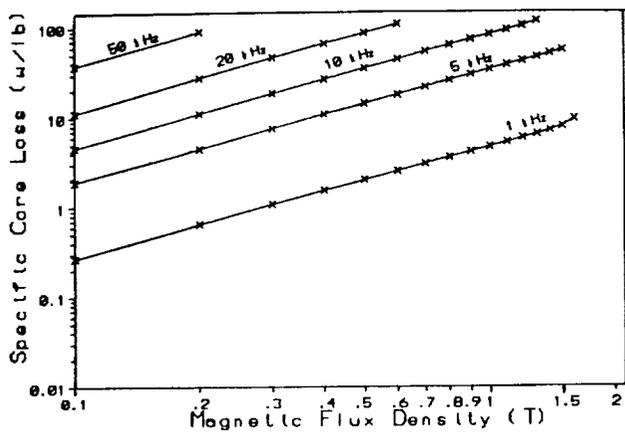
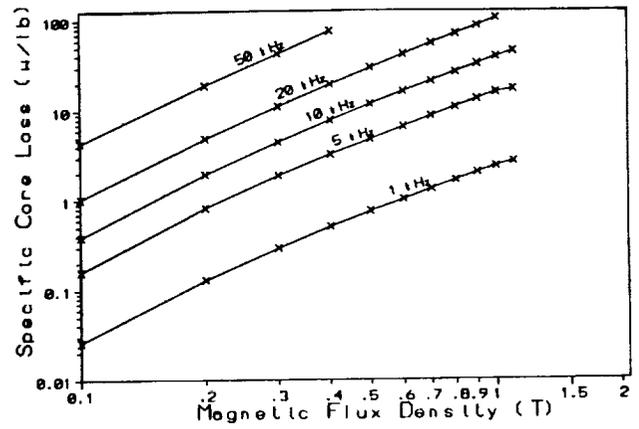


Figure 1. Saturation flux density, B<sub>sat</sub> versus temperature. B<sub>sat</sub> taken from B-H saturation loops at 1 kHz.

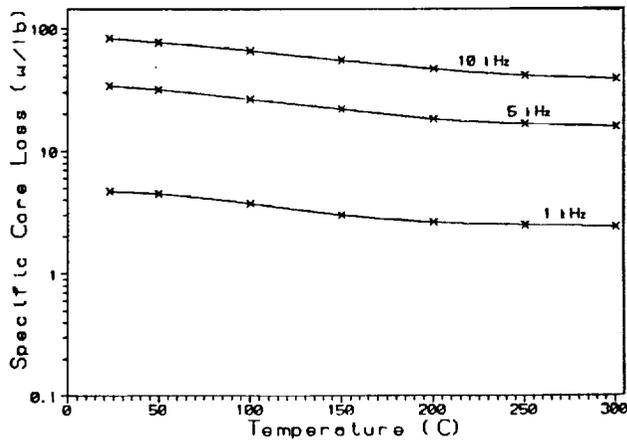


(a)

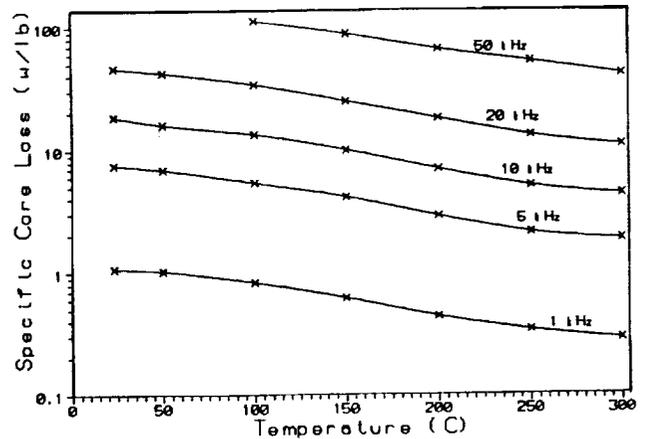


(b)

Figure 2. Oriented - grain 50 Ni-50 Fe specific core loss versus magnetic flux density at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1A-01). (a) T=23 C, (b) T=300 C.

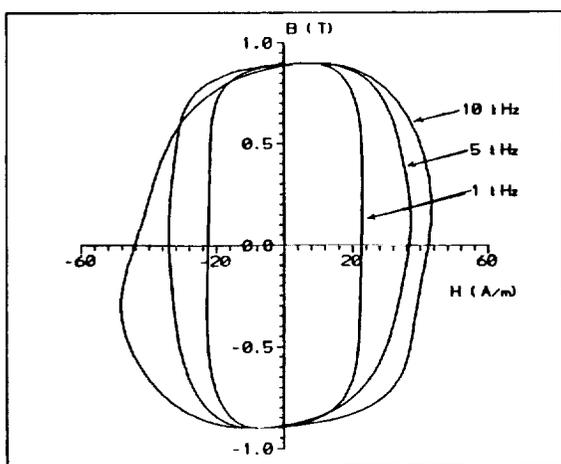


(a)

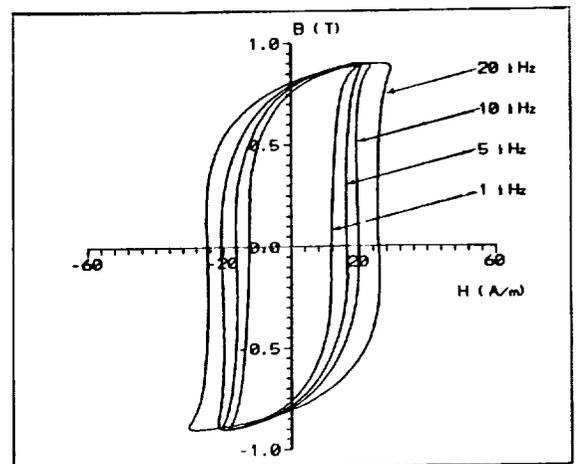


(b)

Figure 3. Oriented - grain 50 Ni - 50 Fe specific core loss versus temperature at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1A-01). (a)  $B_m = 1.0$  T, (b)  $B_m = 0.3$  T.

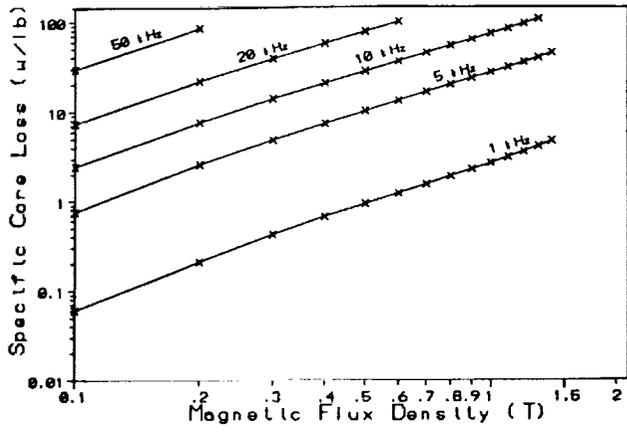


(a)

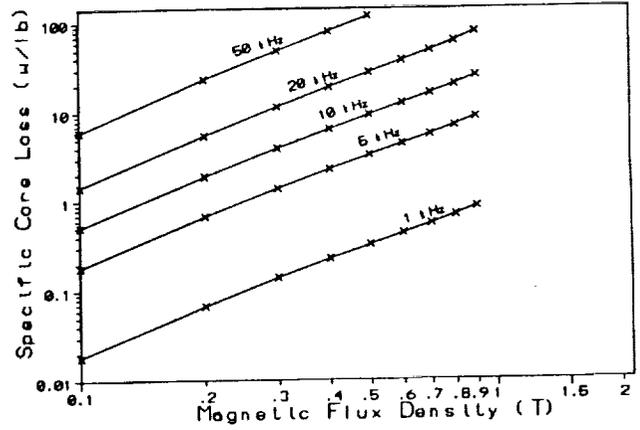


(b)

Figure 4. Oriented - grain 50 Ni - 50 Fe B-H loops for  $B_m = 0.9$  T at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1A - 01). (a) T=23 C, (b) T=300 C.

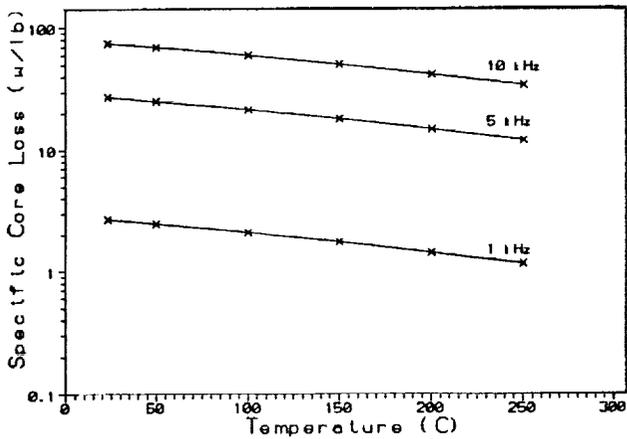


(a)

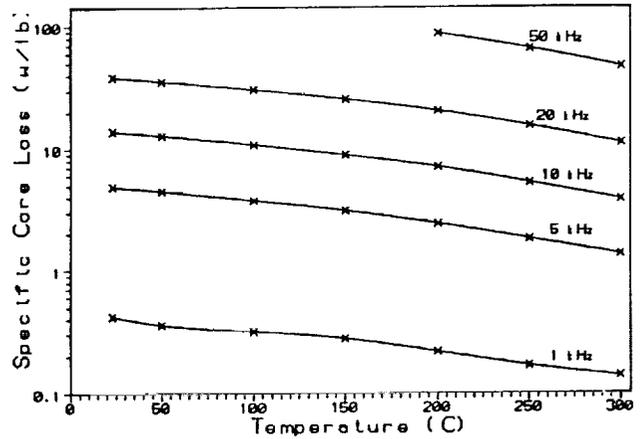


(b)

Figure 5. Nonoriented - grain 50 Ni - 50 Fe specific core loss versus magnetic flux density at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1H-20). (a) T=23 C, (b) T=300 C.

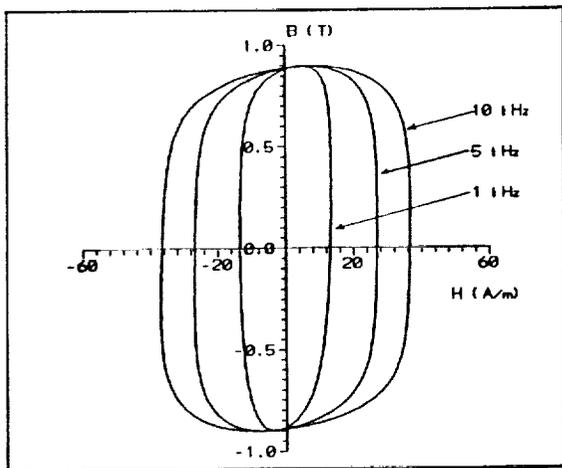


(a)

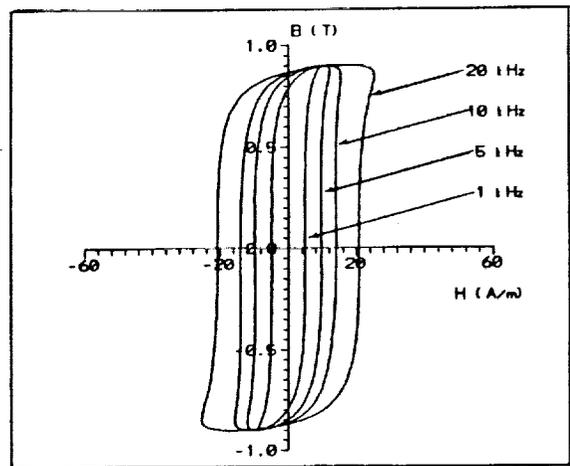


(b)

Figure 6. Nonoriented - grain 50 Ni - 50 Fe specific core loss versus temperature at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1H-20). (a)  $B_m = 1.01$  T, (b)  $B_m = 0.3$  T.

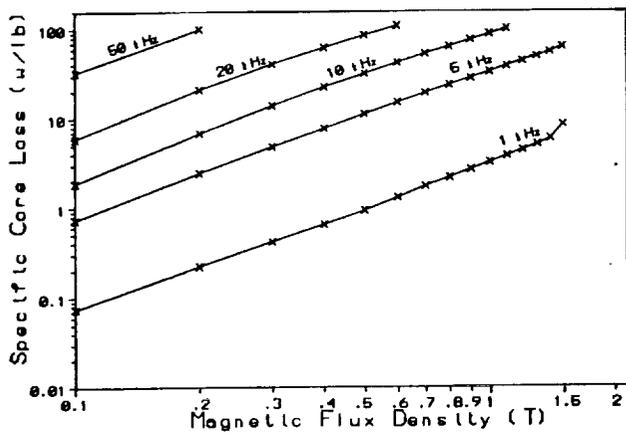


(a)

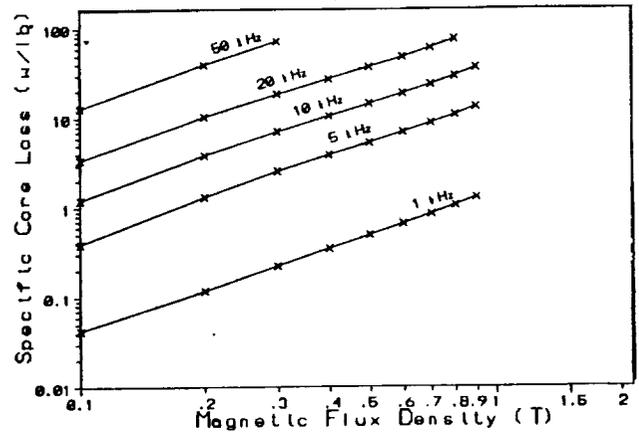


(b)

Figure 7. Nonoriented - grain 50 Ni - 50 Fe B-H loops for  $B_m = 0.9$  T at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1H-20). (a) T=23 C (b) T=300 C.

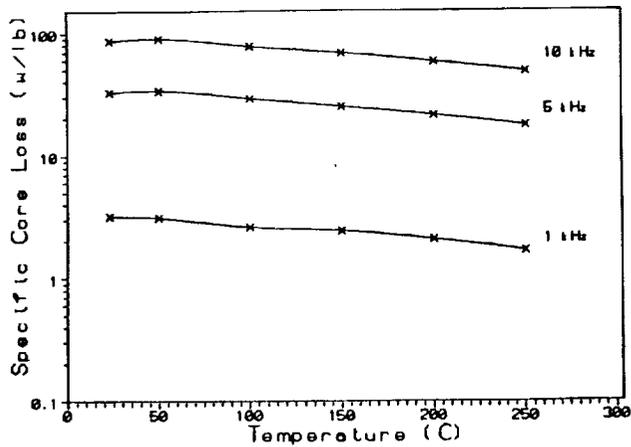


(a)

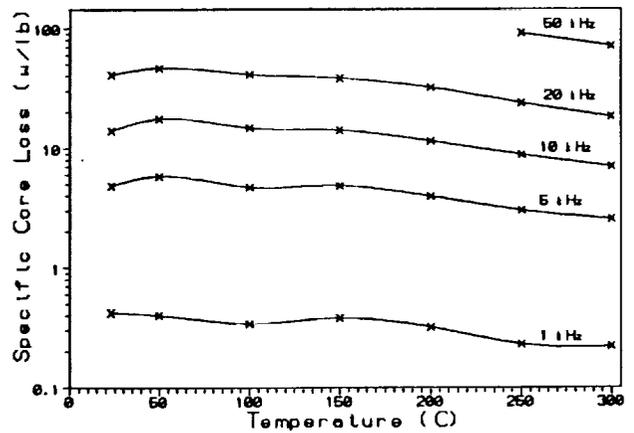


(b)

Figure 8. Metglas 2605SC specific core loss versus magnetic flux density at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 thick tape (1B-03). (a) T=23 C (b) T=300 C.

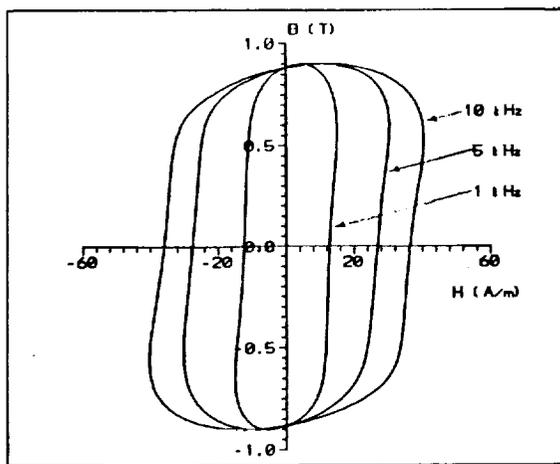


(a)

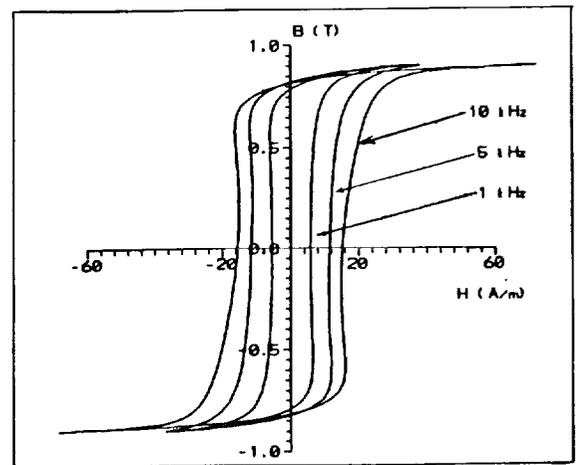


(b)

Figure 9. Metglas 2605SC specific core loss versus magnetic flux density at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1B-03). Bm = 1.0 T, (b) Bm = 0.3 T.



(a)



(b)

Figure 10. Metglas 2605SC B-H loops for Bm = 0.9 T at selected frequencies (sinewave voltage excitation) for toroid wound from 0.001 inch thick tape (1B-03). (a) T=23 C, (b) T=300 C.

**REPORT DOCUMENTATION PAGE**Form Approved  
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

<b>1. AGENCY USE ONLY (Leave blank)</b>		<b>2. REPORT DATE</b> September 1991	<b>3. REPORT TYPE AND DATES COVERED</b> Technical Memorandum	
<b>4. TITLE AND SUBTITLE</b> Comparison of High Temperature, High Frequency Core Loss and Dynamic B-H Loops of Two 50 Ni-Fe Crystalline Alloys and an Iron-Based Amorphous Alloy			<b>5. FUNDING NUMBERS</b>  WU-590-13-31	
<b>6. AUTHOR(S)</b> W.R. Wieserman, G.E. Schwarze, and J.M. Niedra				
<b>7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)</b> National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135-3191			<b>8. PERFORMING ORGANIZATION REPORT NUMBER</b>  E-6515	
<b>9. SPONSORING/MONITORING AGENCY NAMES(S) AND ADDRESS(ES)</b> National Aeronautics and Space Administration Washington, D.C. 20546-0001			<b>10. SPONSORING/MONITORING AGENCY REPORT NUMBER</b>  NASA TM-105205	
<b>11. SUPPLEMENTARY NOTES</b> Prepared for the 26th Intersociety Energy Conversion Engineering Conference cosponsored by ANS, SAE, ACS, AIAA, ASME, IEEE, and AIChE, Boston, Massachusetts, August 4-9, 1991. W.R. Wieserman, University of Pittsburgh at Johnstown, Johnstown, Pennsylvania 15902; G.E. Schwarze, NASA Lewis Research Center; J.M. Niedra, Sverdrup Technology, Inc., Lewis Research Center Group, 2001 Aerospace Parkway, Brook Park, Ohio 44142. Responsible person, G.E. Schwarze, (216) 433-6117.				
<b>12a. DISTRIBUTION/AVAILABILITY STATEMENT</b>  Unclassified - Unlimited Subject Category 33			<b>12b. DISTRIBUTION CODE</b>	
<b>13. ABSTRACT (Maximum 200 words)</b>  The availability of experimental data that characterizes the performance of soft magnetic materials for the combined conditions of high temperature and high frequency is almost nonexistent. An experimental investigation was conducted over the temperature range of 23 to 300 C and frequency range of 1 to 50 kHz to determine the effects of temperature and frequency on the core loss and dynamic B-H loops of three different soft magnetic materials; an oriented-grain 50Ni-50Fe alloy, a nonoriented-grain 50Ni-50Fe alloy, and an iron-based amorphous material (Metglas 2605SC). A comparison of these materials shows that the nonoriented-grain 50Ni-50Fe alloy tends to have either the lowest or next lowest core loss for all temperatures and frequencies investigated.				
<b>14. SUBJECT TERMS</b> Specific core loss; B-H hysteresis loop; High temperature; High frequency; Magnetic measurements; Transformers; Power conditioning			<b>15. NUMBER OF PAGES</b> 8	
			<b>16. PRICE CODE</b> A02	
<b>17. SECURITY CLASSIFICATION OF REPORT</b> Unclassified	<b>18. SECURITY CLASSIFICATION OF THIS PAGE</b> Unclassified	<b>19. SECURITY CLASSIFICATION OF ABSTRACT</b> Unclassified	<b>20. LIMITATION OF ABSTRACT</b>	